

# Conference Summary

## Hydrogen for Sustainable Mobility Forum

### Oct. 17-18, 2023, Torino, Italy

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## Why H<sub>2</sub>-ICE?

Interest in hydrogen fueled internal combustion engines is increasing in major automotive markets, driven by various regulatory and commercial drivers:

- Tailpipe CO<sub>2</sub> regulations for both light- and heavy-duty vehicles : H<sub>2</sub>-ICE offers near-zero tailpipe CO<sub>2</sub>
- Hard-to-electrify segments such as long-haul transport will require alternative solutions
- Provide a market for hydrogen and refueling infrastructure while fuel cell vehicles become more prevalent. H<sub>2</sub>-ICE enables change from conventional fossil fuels while using mostly existing engine hardware.
- H<sub>2</sub> can serve as an energy carrier (or feedstock to other e-fuels) to balance the supply-demand mismatch between regions which can produce and use green electricity.

## Challenges

- Availability of green H<sub>2</sub>: The potential for H<sub>2</sub> to decarbonize transport ultimately rests on the fuel being derived from green sources and not from the current steam methane reforming. The amount of green H<sub>2</sub> produced today is very small compared to the requirement, and the cost is very high.
- NO<sub>x</sub> emissions are produced and will require diesel-like after-treatment. Particulate emissions are low compared to diesel but a filter might be required for European PN standards. H<sub>2</sub> slip needs to be addressed and requires an oxidation catalyst.

## Guest Contribution by Dr. Abdullah Bajwa

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Comparison of H<sub>2</sub> as an ICE fuel to gasoline

| Property                         | Comparison with Gasoline  | Positive Effects   | Negative Effects   |
|----------------------------------|---|--|--|
| Density                          | Lower (0.08 vs 692 kg/m <sup>3</sup> at 300 K and 1 bar [1])                            | High diffusivity and mixing rates  | <ul style="list-style-type: none"> <li>• Low energy density</li> <li>• No vaporisation-induced charge cooling</li> <li>• Limited on-board storage</li> </ul>             |
| Volumetric energy density        | Lower (10.7 vs 33x10 <sup>6</sup> MJ/m <sup>3</sup> at 1 bar and 0°C [7])               |  | Large volume of fuel needed (low power density)  |
| Heating value                    | Higher (LHV: 120 vs 44.3 MJ/kg [1])   | Compensation for low density <sup>a</sup>  |  |
| Laminar Flame Speed <sup>b</sup> | Higher (185 vs 40 cm/s at $\phi = 1$ , 1 bar, 298 K)                                    | <ul style="list-style-type: none"> <li>• Thinner flames and lower minimum ignition energy</li> <li>• Faster / complete combustion</li> <li>• Lower turbulence requirements</li> </ul>                    | Increased peak pressure and pressure rise rate, and wall heat transfer   |
| Minimum ignition energy          | Lower (0.02 vs 0.28 mJ at 300 K, 1 bar [1])   | <ul style="list-style-type: none"> <li>• Wide flammability limits</li> <li>• Hot-surface assisted ignition possibility</li> </ul>  | Surface-ignition (pre-ignition, backfire)  |
| Quench distance                  | Shorter (0.64 vs 2.84 mm at $\phi = 1$ [6])   | More complete combustion   | <ul style="list-style-type: none"> <li>• Increased wall heat transfer (thinning of the thermal boundary layer)</li> <li>• Crevice combustion and backfire [6]</li> </ul> |
| Flammability Limits              | Wider ( $\phi = 0.1-7$ vs 0.66-3.85 at 300 K, 1 bar <sup>c</sup> [1])                   | <ul style="list-style-type: none"> <li>• Ultra-lean combustion</li> <li>• In-cylinder NO<sub>x</sub> abatement</li> <li>• Qualitative load control</li> <li>• Reduced turbulence requirements</li> </ul> | <ul style="list-style-type: none"> <li>• Backfire</li> <li>• Crevice combustion</li> <li>• Crank-case combustion</li> </ul>  |
| Mass diffusivity (in air)        | Higher (0.61 vs 0.07 cm <sup>2</sup> /s at 1 bar and 300 K [1])                         | Faster mixing and combustion   | <ul style="list-style-type: none"> <li>• Thermodiffusive instability</li> <li>• Preferential diffusion instability</li> </ul>  |
| Auto-ignitability                | Unclear (Higher RON, Lower MON, Higher AI temperature, Low methane number) <sup>d</sup> | Higher compression ratios possible   | <ul style="list-style-type: none"> <li>• Long ignition delay</li> <li>• Difficult to initiate diffusive (CI) combustion</li> </ul>                                       |

## Engine Advances

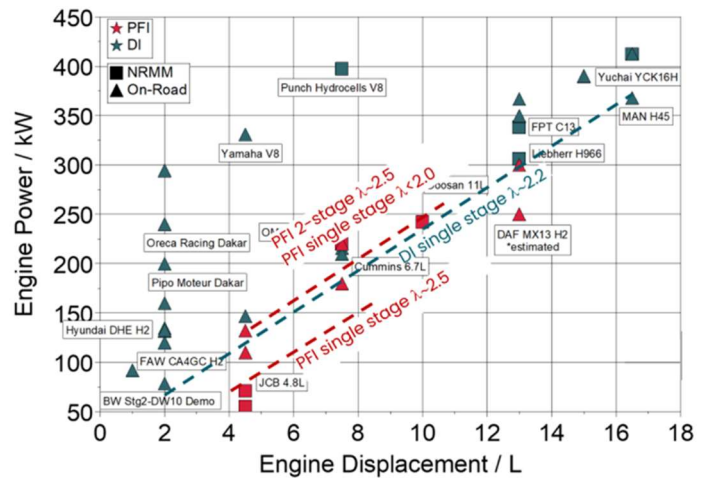
**FEV** showed that 45 different H<sub>2</sub>-ICE engines from 29 different manufacturers are currently being developed, for both on-road and non-road applications. Smaller, light-duty engines are mostly PFI, and larger > 13L engines are mostly DI, while the medium-duty engines have a mix of both technologies.

The key targets for improving H<sub>2</sub>-ICE are performance, emissions and efficiency, and these influence the choice of technologies such as air handling (boost, EGR), fuel injection (PFI, LP-DI, HP-DI), after-treatment (TWC/SCR/PF), engine design and combustion (spark/compression ignition, lean/ultra-lean, compression ratio, etc.)

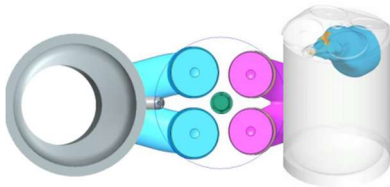
For commercial vehicle applications, low-P DI is favored currently and efficiencies > 44% have been achieved.

**IFPEN** provided an update on the various research activities and capabilities relevant to H<sub>2</sub>-ICE.

- Previous research on a single-cylinder engine has shown that NO<sub>x</sub> emissions can be near-zero at mean air-to-fuel ratio ( $\lambda$ ) of 2.8, increasing non-linearly at  $\lambda < 2.2$ . A consortium of leading suppliers and OEMs is working on developing a dedicated 4 cylinder 2.3L engine for light-duty application. Target is operation at  $\lambda = 2.5$  for very low NO<sub>x</sub> emissions.
- A port-injected, 8L, 6-cylinder engine is being developed for demonstration with a 19-ton truck. Effective efficiency of >40% was achieved and engine-out NO<sub>x</sub> emissions measured at 0.6 g/kWh on the WHTC, an order of magnitude below diesel.



The combination of stoichiometric operation and use of a TWC-only after-treatment is possible as well, as was shown by **Ferrari**, on a 500-cc single cylinder engine with direct injection at 5 – 40 bar. Specific power of 140 kW/l was achieved, and it required the use of port water injection to avoid preignition. Compared to lean combustion, the indicated efficiency is lower for stoichiometric.



CFD modeling capabilities are being used to optimize fuel injection and mixing, both critical for further efficiency gains and emission reduction. As an example, **IAV GmbH** showed that the use of a “jet cap” for injecting fuel can help improve fuel-air mixture homogenization and NO<sub>x</sub> emission reduction by an order of magnitude.

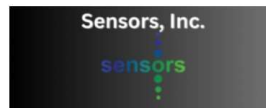
**FPT** presented their Cursor xC13 (13L) prototype H<sub>2</sub>-ICE, developed on a multi-fuel platform for diesel, natural gas and H<sub>2</sub>. The engine uses low pressure (30-40 bar) DI and lean combustion with SCR after-treatment. The engine delivers ~ 475 hp peak power and 2,200 Nm peak torque. Optical diagnostics is being used to evaluate the various root causes of pre-ignition.





No discussion of H<sub>2</sub> is complete without cost considerations of green H<sub>2</sub>. **Punch** showed their analysis which concludes that the cost of H<sub>2</sub> needs to drop to €5/kg to be competitive with diesel. Fuel cell vehicles are more expensive than H<sub>2</sub>-ICE, but their higher efficiency makes the total cost of ownership (TCO) comparable, so expect fuel cells to provide stiff competition. Punch also showed their 6.6L V8 engine, targeting a wide range of applications including gensets and non-road engines. The engine uses port-fuel injected H<sub>2</sub>, along with NO<sub>x</sub> control strategies such as high-P cooled EGR and retarded spark timing.

## Scroll down for NO<sub>x</sub> control – but first a quick “Thank you” to sponsors.

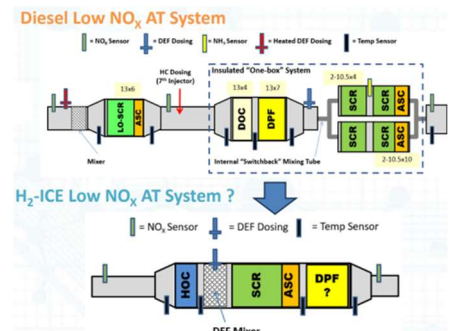


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## NO<sub>x</sub> Control

The current preferred technology for NO<sub>x</sub> control is Cu-SCR, same as for diesel engines. Still, H<sub>2</sub>-ICE will require further optimization to overcome specific challenges. **Southwest Research Institute (SWRI)** is leading an effort in this regard. There is room for simplification and downsizing given the absence of soot emissions, lower engine out NO<sub>x</sub> emissions and lack of hydrocarbon emissions.

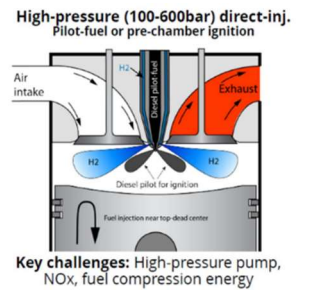
On the other hand, the higher water content is known to adversely affect low temperature SCR conversion. H<sub>2</sub> slip is an issue given the global warming potential of H<sub>2</sub> and increases the propensity for N<sub>2</sub>O emissions.



**AVL** showed the use of stoichiometric operation with water injection as a pathway to achieve similar efficiency as lean combustion, while using a simpler after-treatment. High water content in exhaust can be used to advantage here, with water condensed out from the exhaust using a heat exchanger. Other than a TWC, a passive SCR is added to convert NO<sub>x</sub> using NH<sub>3</sub> generated during rich operation. This  $\lambda=1$  operation with water injection and a late injection strategy was shown to deliver similar power as the reference gasoline engine and achieve 150 kW/l power for a 2L race car engine. For heavy-duty, 50.5% BTE was achieved on a 13L engine using lean

combustion and high-P DI. Increase in compression ratio (to 23:1) and further improved turbocharger efficiency is predicted to raise the BTE to 51.7%.

At the core of this concept is the HPDI fuel injection system, which was discussed in more detail by **Westport Fuel Systems**. It includes a pilot diesel injection to promote ignition, followed by H<sub>2</sub> injection at high pressure. The amount of diesel injection must be optimized to qualify H<sub>2</sub>-ICE as a ZEV in Europe. The use of high P injection is combined with EGR to reduce NO<sub>x</sub>. A “smart tank” using a compressor is required to enable driving ranges > 500 km. Simulations predict a range of 900 km with a smart tank with 80 kg fuel.



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